Modeling and FDTD Simulation of Dispersive, Gyromagnetic Transmission Lines

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**Abstract** –*S*

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# Introduction

Ferromagnetic materials are widely used in bulk power transmission and distribution transformers, elecromechanical machines, power electronic converters and radio frequency communication because their affinity for magnetic flux enables them to conduct magnetic information efficiently. They are mostly used as interfaces between isolated electric circuits which need to communicate at different voltage or current levels. This translation of electromagnetic information between the electric and magnetic domains is not perfect as it incurs energy losses due to Hysteresis, Eddy currents, Skin effect, Proximity effect, Gyromagnetism, Magnetoresistance, Magnetostriction and other residual loss mechanisms. Realistic system level models for the analysis of Ferromagnetic materials must account for this information delay, distortion and attenuation.

As evident from experimentation, Ferromagnetic materials change their channel properties under different mechanical, thermal and electromagnetic stresses. Many researchers have attempted to refine the electromagnetic transmission line model by including frequency dependent permittivity, permeability and conductivity. H. Zhao, Y. Li, Q. Lin, and S. Wang [14] presented a closed form solution for estimating parasitic capacitance of a ferromagnetic core, which stores electric energy in the gradient electric field developed inside the core and is responsible for the high frequency self-resonance and frequency limitation of the magnetic core. The frequency independent power losses due to Ohmic losses were also considered in an equivalent core impedance. J. Xu, M. Koledintseva, Y. Zhang, Y. He, B. Matlin, R. Dubroff, J. Drewniak, and J. Zhang [13] presented an experimental setup for calculating frequency domain behavior of complex permeability and permittivity of a ferromagnetic transmission line. The measured intrinsic impedance and propagation constant was used to determine the per unit length transmission line parameters. H. Al-Barqawi, N. Dib and M. Khodier [1] presented a closed form solution for analyzing the electromagnetic fields in a waveguide filled with an anisotropic, dispersive, gyromagnetic ferrite. The analysis did not account for non-linearity of the magnetic material.

The Electromagnetic Transmission Line model has been used to accurately replicate the behavior of Ferromagnetic materials in electromagnetic simulations. H. Zhao, Y. Li, Q. Lin, and S. Wang [14]. N. Shirdel, A. Akbari, H. Mirzaei, and M. Abrishamian [11] presented a FDTD simulation for propagation of UHF Gaussian pulse partial discharges in a dispersive, anisotropic, conductive ferromagnetic transformer core. J. Xu, M. Koledintseva, Y. Zhang, Y. He, B. Matlin, R. Dubroff, J. Drewniak, and J. Zhang [13] compared with electromagnetic FDTD simulation and analytical results. H. Al-Barqawi, N. Dib and M. Khodier [1] carried out Two Dimensional Finite Difference Time Domain simulation for the structure and the frequency variation of propagation constant was studied for the microwave frequency range.

The Ferromagnetic Transmission Line model must be translated into a system level design which can explain the flow of magnetic flux as the effective magnetic charge due to the application of Magnetomotive force. The electric circuit laws are not applicable to magnetic circuits because they are not designed to conduct electric charge upon application of electromotive force. Many researchers have tried to define magnetic circuit laws which can be applicable to DC and AC magnetic circuits. The most important magnetic circuits are the DC Reluctance model, the low frequency Permeance-Capacitance model and the high frequency Magnetic Transmission Line model.

Magnetic Reluctance circuit model [2], based on the G. Ohm’s Law, depicts magnetic core as a Magnetic reluctance which resists the flow of Magnetic Flux. The Reluctance model is only suitable for low frequency steady state simulations of transformers if the reluctance profile of the magnetic core is already known. It is not power invariant as the Ohm’s Law analogy is ill defined.

R. Buntenbach [2] proposed Power Invariant Permeance-Capacitance Model based on B. Tellegen’s Gyrator Theory. The Permeance-Capacitance model uses a nonlinear permeance to model nonlinearity and hysteresis losses of magnetic materials. The Permeance-Capacitance model is only suitable for low frequency simulations of ferromagnetic materials. J. Allmeling, W. Hammer, and J. Schonberger [2] presented a permeance-capacitance model for a ferromagnetic transformer core. The circuit adopted a gyrator for the transformation between electric and magnetic domains. Nonlinear permeance elements were used to model core hysteresis losses and magnetic flux leakage. A magnetic conductance was used to represent eddy current losses. M. Luo, D. Dujic, and J. Allmeling [9] presented a permeance-capacitance model for a laminated steel ferromagnetic transformer core to model hysteresis losses and frequency dependent eddy current losses. The non-linear core permeance was designed to approximate the results obtained for a low frequency excitation. The model was not valid for high frequency simulations.

J. Faria [4] – [6] presented Magnetic Transmission Line Model based on the conventional Electric Transmission Line Model. For magnetic transmission lines, transverse impedance and the longitudinal admittance determine the propagation constants for the wave modes. Solutions to Electromagnetic equations were presented in the form of a superposition of natural modes of propagation. Simulations showed that they exhibit super-luminal phase velocity and almost zero attenuation dispersion in the microwave frequency range. The Magnetic Transmission Line exhibited the behavior of a high pass filter.

This research attempts to extend the Magnetic Transmission Line Model for the modeling of dispersive, gyrotropic, ferromagnetic transmission lines, and studying the high frequency response of magnetic transmission line parameters.

# Magnetic Transmission Line Model

The Magnetic Transmission Line Model is useful for modeling linear, dispersive ferromagnetic materials. It provides a closed form solution for electric and magnetic parameters using a system level circuit.

Complex permittivity can be represented as:

The real part is responsible for the displacement current, whereas the imaginary part contributes to the conduction current. During Lorentzian resonance, the lattice vibrations of the atomic harmonic oscillators become extreme, and the electric conductance of the magnetic material increases greatly. Hence the material acts like an electric conductor with a very low resistivity. This resonance causes a peak in electric losses.

Complex permeability can be represented as:

Although Magnetic conduction currents do not exist, Magnetic displacement currents can flow inside a magnetic material. During Lorentzian resonance, the real permeability drops, the magnetic displacement currents are restricted and the magnetic susceptibility falls. This causes failure of the magnetic system.

Analogous to the scalar Electric Potential, scalar magnetic potential can be defined as

The Magnetic Displacement Current is defined as the rate of change of magnetic flux :

The per unit length transverse magnetic inductance represents a magnetic Energy storage element storing magnetic flux:

The per unit length longitudinal capacitance represents an Electric Energy storage element storing electric charge:

The per unit length Magnetic conductance dissipates energy due to Hysteresis, Eddy currents, Skin effect, Proximity effect, Piezomagnetism, Magnetoresistance, Magnetostriction and other residual losses. It is closely related to the magnetic reluctance:

The Magnetic Transmission Line Equations are

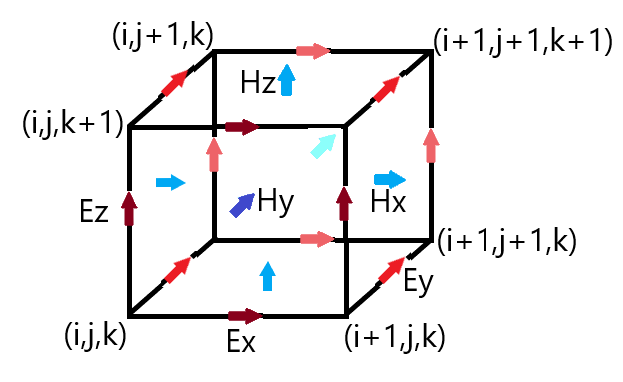
The characteristic impedance is the ratio of Magnetic displacement current to the Magnetic Voltage. It is calculated as

# Finite Difference Time Domain Electromagnetic Simulation

MEEP software was used for the electromagnetic simulation of the Gyrotropic, Dispersive, Ferromagnetic Transmission Lines using the Finite Difference Time Domain method which discretizes Maxwell’s Equations using central difference approximations to the space and time partial derivatives. The different field components at a grid location are stored in the edges and faces of a cubic element called Yee’s Cell. The electromagnetic fields are evolved in discrete time steps using leap frog method.

Faraday’s Law can be discretized as follows:

Similarly, Ampere’s Law can be approximated as follows:



MEEP simulator was used to simulate anisotropic, dispersive and gyromagnetic materials.

1. Dispersion Model

Drude-Lorentzian Model models frequency dependent permittivity and permeability. It explains the electrodynamic properties by regarding conduction band electrons as non-interacting electron gas. When the material is excited by an external source of resonant frequency, the material absorption loss increases greatly. Electromagnetic Energy is converted into other forms of energy. Flux Densities contain terms for infinite frequency response and frequency dependent Polarization vector.

and are represented as a sum of harmonic resonances and a term for frequency independent electric conductivity.

is the electrical/magnetic conductivity. is the oscillator strength, is the angular resonance frequency, is a damping factor.

1. Gyrotropy Model

Landau-Lifshitz-Gilbert model describes the precessional motion of saturated magnetic dipoles in a magnetic field.

describes the linear deviation of magnetization from its static equilibrium value. Precession occurs around this unit bias vector . represents oscillator strength, is the angular resonance frequency, is the oscillator damping factor.

# Simulation Results

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# Discussion

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# Conclusion

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